

# COMPLEX MATHEMATICAL MODEL AND CALCULATION METHOD FOR HIGH EMISSION GAS DISCHARGE HOLLOW CATHODES

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The complex mathematical model and the calculation method are presented, which permit to calculate main local and operation descriptions of high emission gas-discharge hollow cathodes, including the forecast of life-time in steady state operation mode. The mathematical model uses the kinetics description of electrons and electric gas dynamics description of atoms and ions inside the cathode. The state of activator film and surface temperature field are also calculated. Semi-empiric erosion model is based on the thermally stimulated cathode sputtering theory, which is developed by authors.

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The building of mathematical models of base degradation parameters (BDP) change is one of the most important tasks, which are solved while the developing of fast test methods.

The creation of quantitative mathematical models of hollow cathodes, which permit to realize the optimal work routines and to forecast their life-time, is complex and actual task.

The complete and precise mathematical model is necessary for the development of life-time design methods, which describe the temporal evolution of main work routines, which are responsible for reliability and life-time.

The complex mathematical model of high emission gas discharge hollow cathodes (HEGHC) is developed firstly in Science and Technology Center of Space Power and Engines in KhAI [1 - 5], which differs by completeness and precision of description of work routines determining HEGHC emission ability, erosion strength. This model permits with enough for design practice precision to make the calculations and forecast of main local and integral HEGHC descriptions, including life-time.

This model includes the space-kinetic diffusion model of processes, which considers the plasma components dynamics inside the hollow, electron spectrum features, activator dynamics, Langmuir layer descriptions, energy transfer between the surface and the volume, processes in external discharge column; the model of film thermal emitters work; erosion model, which is built on the heat stimulated cathode sputtering (HSCS) theory (Fig. 1).

The complex non-linear mode of surface and volume processes mutual influence was taken into consideration. The expressions for ion surface recombination, electron back current, emission were used like the boundary conditions for plasma dynamics equations. Plasma descriptions on Langmuir border were in turn included into boundary conditions.

The critical expression was used in boundary conditions on Langmuir border:

$$m_e V_e^2 + m_i V_i^2 = k(T_e + T_i). \quad (1)$$

This condition can be realized either in the most thin flow section (exit orifice) or because of quasi neutrality break-up (inside Langmuir layer).

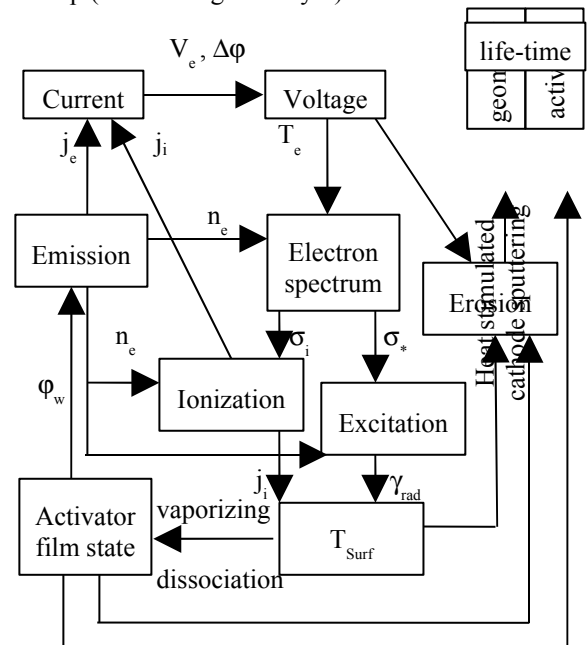


Fig. 1. Complex model structure

The emission current depends on the state of activator film. The equations describing the activator dynamics in the volume and on the surface were also considered like mutual boundary conditions. Also activator dynamics and emission currents depend on temperature surface distribution, which in turn is determined on heat flow from the volume. The rate of ionization and excitation as well as electron back current density depends on the peculiarities of electron energy distribution in high energy area.

According to these ideas the complex model includes the following sub-models:

- the processes inside hollow main volume;
- the processes near the orifice;
- Langmuir cathode layer;
- electrons energy distribution;
- heat stimulated cathode sputtering;
- film thermal emitter work and activator dynamics;
- cathode surface temperature distribution;
- external column.

The complex models unites the continuum methods (in the tasks of electric field and plasma components space behavior) and kinetics approach (in the task of electron energy distribution).

It is shown that the main collision factors, which must be considered in plasma components space dynamics, are ion mass flow velocity decrease and velocity dispersion (temperature) increase due to appearance of new ions inside already accelerated ones because of ionizations. We have named these factors like "ionization deceleration" and "ionization heating".

Electron energy distribution plays the most important role in these model. The kinetics equation in diffusion

approximation (Landau mode for collision integral) is

$$\mathbf{v} \cdot \nabla f(\vec{v}) + \frac{e}{m_e} \nabla \varphi \cdot \nabla_v f(\vec{v}) = \frac{\delta f(\vec{v})}{\delta t} \quad (2)$$

with Landau collision integral:

$$\left( \frac{\delta f(v)}{\delta t} \right)_{e-e} = -\frac{1}{v^2} \frac{\partial}{\partial v} (v^2 \Gamma(v)) \quad (3)$$

where initial form of electron flow density in velocity space is:

$$\Gamma(v) = \int_0^\infty \int_0^\pi \int_0^{2\pi} \int_0^\infty \int_0^\pi \int_0^{2\pi} \int_{v-\delta v}^v [f(v'')f(v') - f(v'+\delta v)f(v'-\delta v)] |v'' - v'| \times \dots \quad (4)$$

which can be reduced, taking into consideration the descriptions of processes, into Landau form:

$$\Gamma(v) = \frac{32}{3} \pi^2 \sigma_e \left[ \frac{e\varphi_i}{m_e} \right]^2 \times \int_0^\infty \left[ \frac{f(v)}{v'} \frac{d f(v')}{d v'} - \frac{f(v')}{v} \frac{d f(v)}{d v} \right] \times \text{Min}^3(v, v') v' d v' \quad (5)$$

Other main part of complex model is erosion sub-model based on HSCS theory. Surface atoms flow in this theory is considered as a result of both ion bombardment and surface atoms thermal oscillations with sputter coefficient, which is the function of ion energy and surface temperature:

$$\Gamma_p = P(\varepsilon_i, T) \Gamma_i \quad (6)$$

The sputter coefficient is calculated using the atoms oscillation faze distribution, velocity direction and value distributions:

$$P(\varepsilon_i, T) = \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} \int_0^{2\pi} \int_{v_{\min}}^{v_{\max}} f(\vartheta) f(\varphi) f(v) \sin \vartheta d\vartheta d\varphi v \quad (7)$$

where

$$v_{\min} = \sqrt{\frac{2\varepsilon_m}{m}} - \sqrt{\frac{2\beta\varepsilon_i}{m}} \cos \vartheta \cos \varphi \quad (8)$$

and

$$v_{\max} = \sqrt{\frac{2\varepsilon_m}{m}} \quad (9)$$

where  $\varepsilon_m$  is the energy of surface atoms desorbtion.

Reply function  $\beta$  here must be taken from experimental data for short-term cathode tests and then be used for long-term life-time forecast.

The calculation results for voltage and orifice radius evolution are shown in Fig. 2 and Fig. 3.

Test and forecast results (Fig. 4) for orifice radius evolution had demonstrated good coincidence.

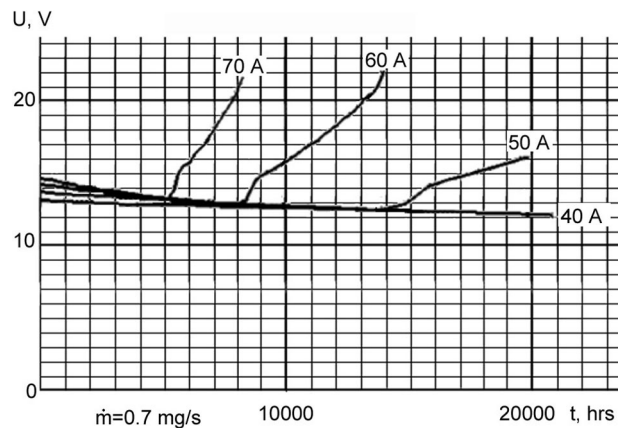


Fig. 2. Voltage evolution forecast

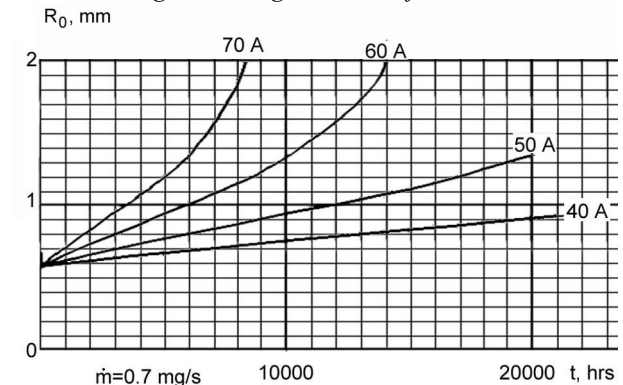


Fig. 3. Orifice radius evolution forecast

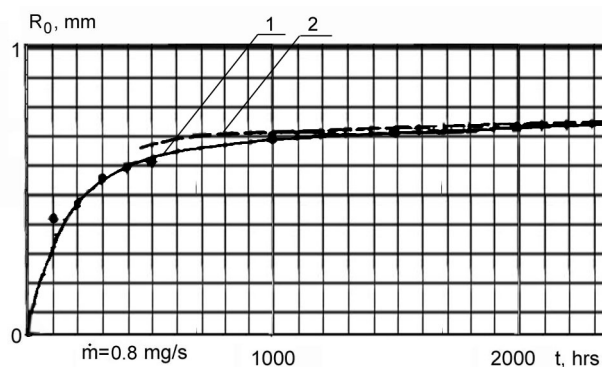


Fig. 4. Test (1) and forecast (2) results

Thus, the models and software developed permit:

- to make life-time design of HEGHC via optimization by the necessary life-time criterion;
- to make the calculation of evolution of cathode main work descriptions;
- to create calculation-experiment methods of HEGHC life-time tests.

#### REFERENCES

1. A.I. Oranskiy. The Method and the Results of Electric Propulsion Thrusters Hollow Cathodes Calculation // *Aerospace Engineering and Technology*: Coll. Papers of State Aerospace University "KhAI", Kharkiv: KhAI, 1998. Iss. 5, p. 229-232 (in Russian).
2. A.I. Oranskiy. Space-kinetic Diffusion Model of Processes in High Emission Gas Discharge Hollow Cathodes // *Aerospace Engineering and Technology*: Coll. Papers of State Aerospace University "KhAI", Kharkiv: KhAI, 1998. Iss. 7, p. 114-117 (in Russian).
3. A.V. Zakhartchenko, S.Yu. Nesterenko, A.I. Oranskiy. The Forecasting of Hollow Cathodes Life-time Properties // *Aerospace Engineering and Technology*: Coll. Papers of State Aerospace University "KhAI", Kharkiv: KhAI, 1997, p. 239-244 (in Russian).
4. N.V. Belan, S.Yu. Nesterenko, A.I. Oranskiy. The Method and the Results of Electrons Energy Distribution Function Calculation inside the Activated Throated Hollow Cathode // *Aerospace Engineering and Technology*: Coll. Papers of Kharkiv Aviation Institute, Kharkiv: KhAI, 1995, p. 184-192 (in Russian).
5. S.Yu. Nesterenko, A.I. Oranskiy. The Mechanism of Cathode Sputter in Low Voltage Hollow Cathode Discharge // *Abstracts of VI All-Union Conf. on Plasma Accelerators and Ion Injectors*. Dnepropetrovsk, 1986, p.58 (in Russian).

### КОМПЛЕКСНАЯ МАТЕМАТИЧЕСКАЯ МОДЕЛЬ И МЕТОДИКА РАСЧЕТА ВЫСОКОЭМИССИОННЫХ ГАЗОРАЗРЯДНЫХ ПОЛЫХ КАТОДОВ

*С.Ю. Нестеренко, А.И. Оранский*

Представлены комплексная математическая модель и методика расчета, позволяющие рассчитывать основные локальные и эксплуатационные характеристики газоразрядных полых высокоэмиссионных катодов, включая прогноз их ресурса в стационарном режиме работы. Математическая модель использует кинетическое описание электронов и электрогазодинамическое описание атомов и ионов в катод. Также рассчитывается состояние пленки активатора и поле температуры поверхности. Полуэмпирическая модель эрозии базируется на разработанной авторами теории термостимулированного катодного распыления.

### КОМПЛЕКСНА МАТЕМАТИЧНА МОДЕЛЬ І МЕТОДИКА РОЗРАХУНКУ ВИСОКОЕМІСІЙНИХ ГАЗОРАЗРЯДНИХ ПОРОЖНИСТИХ КАТОДІВ

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Представлено комплексну математичну модель і методику розрахунку, які дозволяють розраховувати основні локальні та експлуатаційні характеристики газоразрядних порожнистих високоемісійних катодів, включаючи прогноз їх ресурсу в стаціонарному режимі роботи. Математична модель використовує кінетичне описання електронів і електрогазодинамічне описання атомів і іонів в катоді. Також обчислюються стан плівки активатору і поле температури поверхні. Напівемпірична модель ерозії базується на теорії термостимульованого катодного розпилю, що розроблена авторами.